

Optimal Protection Coordination of over current Relays in DG System with Solid State Fault Current Limiters

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Article Info

Volume 82

Page Number: 5442 - 5449

Publication Issue:

January-February 2020

Abstract:

In order to meet the increase in the power demand, Distributed Generation (DG) system plays a major role. Apart from generation it also faces many technical challenges, loss of harmonic control, voltage regulation and losses and changes in the relay coordination due to differences in short-circuit levels. In a system when a short circuit takes place it leads to severe damage as very high magnitude of fault current will be observed. These high magnitude short circuit fault currents eventually leads to coordination problem of Over current relays. To achieve proper coordination, time settings between the relays are optimized using several optimization techniques.

In present circumstances, occurrence of fault in a system have become high which greatly affect reliability of power system. To avoid discontinuities in the system, optimal relay time settings have to be determined which are associated with the fault current that has to be minimized. Here, in order to limit the transient fault current in the system, solid state fault current limiter (SSFCL) is designed. To determine the optimal relay time settings, a new optimization technique, hybrid PSO-GSA is applied.

The reduction in the fault current magnitudes have been observed: without and with SSFCL. Proposed optimization technique has been evaluated by comparing the results for the system with and without DG. The programming is done in MATLAB software and was implemented on 4bus DG system in SIMULINK platform.

Keywords: Distributed Generation (DG), Gravitational Search Algorithm (GSA), Solid State Fault Current Limiter (SSFCL), Hybrid Particle Swarm Optimization-Gravitational Search Algorithm (PSO-GSA).

Article History

Article Received: 18 May 2019

Revised: 14 July 2019

Accepted: 22 December 2019

Publication: 27 January 2020

I. Introduction

Energy requirement in the world has been increasing at a faster rate which is achieved

by placing DG into the system [1]. To achieve reliability of the power system protection coordination plays a vital part.

However, when DG is incorporated then the system undergoes several changes, due to differences in fault current magnitude and the bidirectional flow of power causes relay coordination problem [2].

Radial system is most widely used type of distribution system. Among various protective devices, relays assure faster operation, low maintenance and long durable life where Overcurrent relay protection plays a major role. To achieve proper coordination between the relays, the time settings of the relays have to be determined accurately so that primary relay senses and operates first as soon as the fault occurs. The optimal values of Time setting Multiplier (TMS) and Plug Setting (PS) have to be determined to minimize the relays total operating time. Objective function considered here is a constrained optimization where certain bounds are kept on values of pick up current, plug setting and operating times of relays which is briefly discussed in section 2.

To limit the effect of DG on OC relay coordination, Solid State Fault Current limiter is used to stabilize the system operation. During fault condition, it reduces the fault current magnitude to an acceptable value. And in addition, Particle Swarm Optimization- Gravitational Search Algorithm (PSOGSA) was implemented in order to determine the optimal time settings.

II. Proposed Solid State Fault Current Limiter:

At normal operating state, SSFCL has low voltage drop, less power loss and it inserts low impedance to the system. Whereas if a

fault occurs then it reduces high magnitude transient fault current and provides high impedance to the network. It is required to withstand the fault condition for a sufficient time. It improves power quality and stability of the system. Modeling of SSFCL as in Fig.2.1 consistsof control system which is needed to generate triggering pulses for thyristors[3],[4].Fault Current identification is performed by estimating the preset value of current with that of the RMS value.

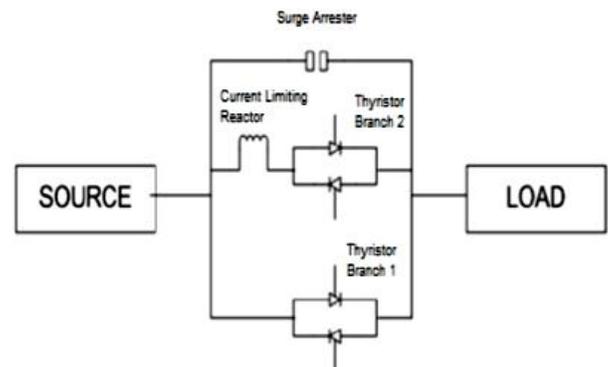


Fig.2.1. Arrangement of SSFCL

The design of SSFCL primarily constitute two solid state switches connected in inversely parallel manner [5]. One pair consists of thyristors whereas the other one consists of thyristor with current limiting reactor in series which limits the detected fault current to a reasonable value [6]. To minimize the effects of switching overvoltage surges on the system, a surge arrester is placed in parallel. To place the current limiting reactor in the system, its value has to be determined. Its value is obtained by equalizing the FCL impedance magnitude with the inductive reactance of the limiting reactor.

$$|Z_{FCL}| = |\omega L_{FCL}| = \frac{\bar{V}}{I_{FCL}} \quad (1)$$

Where, L_{FCL} is limiting reactor inductance, Z_{FCL} is limiting reactor impedance, I_{FCL} is the fundamental fault current, \bar{V} is the phase voltage magnitude.

OC Relay coordination in radial system:

To maintain reliability of the system, proper coordination has to be achieved between the relays. Whenever a fault occurs at a particular point, relay nearer to that point should operate first and remove it as fast as possible. So, the main objective function is to obtain the minimal operating time of relay [7],[8] which is given as,

$$\text{Min } s = \sum_{i=1}^n t_{i,k} \quad (2)$$

Where, $t_{i,k}$ is i th relay operating time for fault in k th zone and n is total number of relays present in the system.

where, t_{op} is operating time of relay, PS is the plug setting of relay, TMS is relay time multiplier setting, I_{relay} is reduced magnitude of fault current seen by relay, and CT sec rated is the CT secondary rated current. Here, IDMT relay is considered whose characteristic values are γ is 0.02, and λ is 0.14. The values of TMS and PS are found using hybrid PSO-GSA.

III. Over Current Relay Coordination through Optimization Techniques:

3.1 Gravitational Search Algorithm (GSA):

GSA is a population-based heuristic algorithm which depends on law of gravity and mass interactions. Agents, which are

Limits on pick up current:

Maximum value of load current observed by each operating relay determines minimum value of relay operating current which is termed as pick up current and vice versa. Bounds are also kept on relay plug setting so that it is maintained between maximum and minimum values.

$$I_{pmin} \leq I_p \leq I_{pmax}$$

$$P_{Smin} \leq P_S \leq P_{Smax} \quad (3)$$

2.1.2 Characteristics of relay:

$$t_{op} = \frac{\lambda (TMS)}{(PSM)^{\gamma-1}} \quad (4)$$

$$t_{op} = \frac{0.14(TMS)}{\left(\frac{I_{relay}}{PS} * CT \text{ sed rated}\right)^{0.02-1}} \quad (5)$$

termed as solutions, interact with other agents with gravitational force. In a particular population the activity of each agent is determined by their own mass where all of them are defined to have variable mass [9]. Best solution is obtained for the object having heavier mass. Controllability of velocity of a body is assured by these masses. After evaluating all the agents in a population best and the worst agents are assigned. The fitness value determined evaluates the values of these parameters [10].

3.2 Particle Swarm Optimization (PSO):

It is a population-based technique based on intelligence and swarm movement. Each

individual is termed as particle and group of particles constitute swarm. These particles move around through the solution space, searching for the best value [11]. With reference to distance between its positional best and current position and, the distance between its current position and its global best; each and every particle in the search space attempts to modify its current position.

3.3 Hybrid PSOGSA:

Hybridization procedure of any two algorithms will be done at a high level or low level with relay or co-evolutionary method which is known as homogeneous or heterogeneous [12]. Here, PSO and GSA are hybridized with the help of a low-level co-evolutionary heterogeneous hybrid technique. The main aim of developing hybrid PSOGSA is to combine the global search capability (g_{best}) in PSO with the local search capability (p_{best}) in GSA. As the functionality of both algorithms is combined, hybrid here is low level. Both the algorithms run in parallel hence it is known as co-evolutionary. To achieve hybridization, agents which are known to be candidate solution will be initialized first. When a better solution is obtained, the agents near the solution attempt to attract the remaining other agents. Finally all the agents move slowly when they combinedly approach nearer to a good solution. In hybrid PSOGSA, each agent has the capability to identify the so far obtained best solution, finally it starts to move towards the best solution. From the obtained values of acceleration, mass and force between the agents, velocity and position are updated

which are calculated from PSO. In this manner, hybridization of two algorithms is carried out.

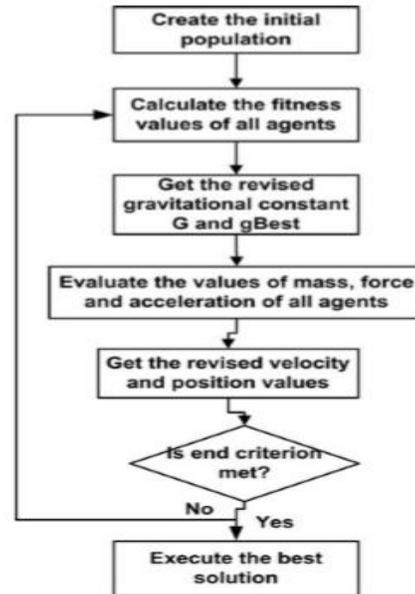


Fig.3.1 Hybrid PSOGSA Flowchart

IV. Simulation Results:

A four bus DG system was modeled to evaluate and minimize the effects of DG on over current relay coordination. The CT ratios of relays present in the system are given below.

Table: I Relay CT Ratio

| Relay | Ratio of CT(A) |
|-------|----------------|
| 1 | 1000/1 |
| 2 | 800/1 |
| 3 | 600/1 |
| 4 | 600/1 |
| 5 | 600/1 |
| 6 | 600/1 |

Table: II LINE DATA:

| Parameter | Value |
|--------------|-------|
| Grid MVA | 25MVA |
| Grid Voltage | 161KV |
| Line length | 100km |

| | |
|-------------------------------|--------|
| Nominal frequency | 50Hz |
| Transformer primary voltage | 161KV |
| Transformer secondary voltage | 11KV |
| Current limiting reactor | 9.95mH |

Various cases have been considered to all of which SSFCL is placed and reduction in the fault current magnitude is observed.

Four cases have been studied where to each case SSFCL is applied to determine the new fault current values for which a hybrid optimization technique PSO GSA is applied to determine TMS and PS values.

Table : III Values of Fault current without and with SSFCL

| Case | Without SSFCL | With SSFCL |
|--|----------------------------|------------------------------|
| 1. Without DG (1) R1 (2) R2 | 2552 A 66.13A | 0.7217A 0.03129A |
| 2. With DG at 20% (1) R1 (2) R2 | 2336A 2800A | 0.7531A 4.106A |
| 3. DG at 23.3% (1) R4 (2) R1 (3) R2 | 675.3A 610.1A 210A | 0.9796A 1.146A 0A |
| 4. DG at 26.6% (1) R4 (2) R1 (3) R2 | 875.3A 610.1A 210.1A | 0.1631A 1.435A 0.1866A |
| 5. DG at 30% (1) R4 (2) R1 (3) R3 | 120A 500A 500A | 0.2847A 0.6946A 0.146A |

Table: IV Relay operating time for fault at different location (without dg)

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 1.34 | - | - | - |
| B | 2 | 0.68 | 1 | 1.63 | 0.95 |
| C | 3 | 0.96 | 2 | 1.62 | 0.66 |
| D | 4 | 1.33 | 1 | 1.64 | 0.31 |
| E | 5 | 1.32 | 2 | 1.63 | 0.31 |
| F | 6 | 1.88 | 3 | 2.20 | 0.32 |

When SSFCL is placed in the system, fault current magnitude is reduced and a new objective function is developed implementing hybrid PSO GSA technique through which better coordination between relays have been observed in table V and VII.

Table: V Relay operating time for different fault location (without dg) observed with hybrid PSO GSA by placing SSFCL

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 0.67 | - | - | - |
| B | 2 | 0.32 | 1 | 0.05 | 0.28 |
| C | 3 | 0.04 | 2 | 0.38 | 0.34 |
| D | 4 | 0.65 | 1 | 0.67 | 0.02 |
| E | 5 | 0.03 | 2 | 0.38 | 0.35 |
| F | 6 | 0.35 | 3 | 0.44 | 0.09 |

Table: VI Relay operating time for different fault location (with DG at 20% level)

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 1.27 | - | - | - |
| B | 2 | 0.67 | 1 | 1.27 | 0.60 |
| C | 3 | 0.36 | 2 | 1.01 | 0.65 |
| D | 4 | 0.49 | 1 | 1.25 | 0.76 |
| E | 4 | 0.49 | 2 | 0.95 | 0.46 |
| F | 5 | 0.50 | 2 | 1.01 | 0.51 |
| F | 6 | 0.62 | 3 | 0.97 | 0.35 |

Table :VIIRelay operating time for system with DG at 20% level along with SSFCL observed with hybrid PSO GSA

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 0.90 | - | - | - |
| B | 2 | 0.77 | 1 | 0.90 | 0.12 |
| C | 3 | 0.13 | 2 | 1.26 | 1.13 |
| D | 4 | 0.58 | 1 | 0.90 | 0.32 |
| E | 5 | 1.12 | 2 | 0.77 | 0.34 |
| F | 6 | 0.53 | 3 | 0.83 | 0.30 |

Table: VIIIRelay operating time at 23.3% DG level

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 1.0225 | - | - | - |
| B | 2 | 0.7496 | 1 | 1.0533 | 0.3037 |
| C | 3 | 0.4809 | 2 | 0.7824 | 0.3015 |
| D | 4 | 0.5619 | 1 | 1.0522 | 0.4903 |
| E | 5 | 0.4013 | 2 | 0.7824 | 0.3811 |
| F | 6 | 0.2278 | 3 | 0.5310 | 0.3032 |

Table: IX Relay operating time at 26.6% DG level

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 0.9890 | - | - | - |
| B | 2 | 0.6902 | 1 | 1.0050 | 0.3148 |
| C | 3 | 0.4544 | 2 | 0.7706 | 0.3162 |
| D | 4 | 0.3573 | 1 | 1.0142 | 0.6569 |
| E | 5 | 0.3762 | 2 | 0.7753 | 0.3991 |
| F | 6 | 0.2299 | 3 | 0.5453 | 0.3154 |

Table: XRelay and CTI values when DG action is not taking place

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 0.4812 | 2 | - | - |
| B | 2 | 0.5592 | 1 | 0.5010 | -0.0582 |
| C | 3 | 0.5499 | 2 | 0.5792 | 0.0293 |
| D | 4 | 0.3127 | 1 | 0.5010 | 0.1883 |
| D | 4 | 0.3127 | 2 | - | - |
| E | 5 | 0.4757 | 2 | 0.6443 | 0.1686 |
| F | 6 | 0.4473 | 3 | 0.5498 | 0.1025 |

In the above table X, CTI is violated. It is observed that for fault at D, E, F, it is a

positive value which means the relays are able to isolate the fault. But for the cases where fault is created at locations A,B and C relay is not able to isolate the fault.

Similarly, for 26.6% penetration CTI values have been observed for LL and LLG fault in below table XI and table XII

Table: XI Relay operating time and CTI values at 26.6% DG level when LL fault occurs

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 0.7382 | - | - | - |
| B | 2 | 0.4751 | 1 | 0.7938 | 0.3187 |
| C | 3 | 0.3217 | 2 | 0.6127 | 0.2910 |
| D | 4 | 0.3075 | 1 | 0.7938 | 0.4863 |
| E | 5 | 0.3427 | 2 | 0.5116 | 0.1689 |
| F | 6 | 0.2142 | 3 | 0.4985 | 0.2843 |

Table.XIIRelay operating time and CTI values at 26.6% DG when LLG fault occurs

| Fault Point | Primary Relay Unit | | Back Up relay Unit | | CTI(sec) |
|-------------|--------------------|----------------|--------------------|----------------|----------|
| | Relay No. | Operating Time | Relay No. | Operating Time | |
| A | 1 | 0.7270 | - | - | - |
| B | 2 | 0.4691 | 1 | 0.7938 | 0.3247 |
| C | 3 | 0.3015 | 2 | 0.5110 | 0.2095 |
| D | 4 | 0.3041 | 1 | 0.7938 | 0.4897 |
| E | 5 | 0.3354 | 2 | 0.5079 | 0.1725 |
| F | 6 | 0.2127 | 3 | 0.4887 | 0.2760 |

Table : XIII Relay TMS and PS values using PSO and GSA (without DG)

| Relay No. | TMS | PS |
|-----------|--------|--------|
| 1 | 0.0840 | 0.9985 |
| 2 | 0.0800 | 1.0742 |
| 3 | 0.0800 | 1.2461 |
| 4 | 0.0803 | 1.1453 |
| 5 | 0.0919 | 1.1011 |
| 6 | 0.0801 | 1.0427 |

Total Operating Time (sec) using PSO 15.0026

| Relay No. | TMS | PS |
|-----------|--------|--------|
| 1 | 0.1065 | 0.9924 |
| 2 | 0.0915 | 1.0018 |
| 3 | 0.1022 | 0.9955 |
| 4 | 0.1426 | 1.0919 |
| 5 | 0.0811 | 1.2316 |
| 6 | 0.0800 | 1.0202 |

Total Operating Time (sec) using GSA 14.5621

Table: XIVRelay TMS and PS values using GSA and PSO at 20% DG level

| Relay No. | TMS | PS |
|-----------|--------|--------|
| 1 | 0.0994 | 0.9275 |
| 2 | 0.1105 | 0.9292 |
| 3 | 0.1001 | 1.4399 |
| 4 | 0.0815 | 1.2607 |
| 5 | 0.1382 | 1.4144 |
| 6 | 0.0893 | 1.0374 |

Total Operating Time (sec) using GSA 9.2148

| Relay No. | TMS | PS |
|-----------|--------|--------|
| 1 | 0.1160 | 0.9179 |
| 2 | 0.0947 | 1.1522 |
| 3 | 0.1125 | 1.2630 |
| 4 | 0.2619 | 0.9106 |
| 5 | 0.0800 | 1.4318 |
| 6 | 0.0801 | 1.1449 |

Total Operating Time (sec) using PSO 10.7

Table: XVRelay TMS and PS values using GSA and PSO techniques at 23.3% DG level

| Relay No. | TMS | PS |
|-----------|--------|--------|
| 1 | 0.2882 | 0.1603 |
| 2 | 0.2227 | 0.1250 |
| 3 | 0.1323 | 0.2225 |
| 4 | 0.1285 | 0.2875 |
| 5 | 0.1060 | 0.2347 |
| 6 | 0.0801 | 0.1117 |

Total Operating Time (sec) using GSA 7.6

| Relay No. | TMS | PS |
|-----------|--------|--------|
| 1 | 0.3928 | 0.1003 |
| 2 | 0.2617 | 0.1037 |
| 3 | 0.1977 | 0.1201 |
| 4 | 0.1142 | 0.1808 |
| 5 | 0.0958 | 1.2928 |
| 6 | 0.0829 | 1.1529 |

Total Operating Time (sec) using PSO 8.1060

Table: XVIRelay TMS and PS values using GSA and PSO techniques at 26.6% DG level

| Relay No. | TMS | PS |
|-----------|--------|--------|
| 1 | 0.3380 | 0.1034 |
| 2 | 0.1792 | 0.1648 |
| 3 | 0.1248 | 0.2594 |
| 4 | 0.1271 | 0.1303 |
| 5 | 0.1076 | 0.2217 |
| 6 | 0.0831 | 0.1187 |

Total Operating Time (sec) using GSA 7.3090

| Relay No. | TMS | PS |
|-----------|--------|--------|
| 1 | 0.2933 | 0.1436 |
| 2 | 0.1827 | 0.1639 |
| 3 | 0.1282 | 0.2523 |
| 4 | 0.0841 | 0.3908 |
| 5 | 0.0969 | 0.3502 |
| 6 | 0.0802 | 0.1344 |

Total Operating Time (sec) using PSO 7.5151

V. Conclusion:

The effect of DG penetration on over current relay coordination was studied. Due to the presence of DG in the system, increased fault current magnitude was reduced by placing SSFCL in the system. The main objective function here is to reduce the relay operating time by determining the optimal time settings of over current relays. This is

achieved by implementing hybrid PSO-GSA technique on a four bus DG system and comparative analysis is done between PSO, GSA and hybrid PSO-GSA techniques. It was observed that the relay operating time was minimum when hybrid PSO-GSA technique was applied to the system.

REFERENCES:

1. P. P. Barker and R.W. de Mello, "Determining the impact of distributed generation on power systems part I - Radial distribution systems," IEEE Trans. Power Del., vol.15, pp.486-493, Apr. 2000.
2. A. Srivastava, J. M. Tripathi, Ram Krishnan and S.K. Parida, "Optimal Coordination of Overcurrent relays using Gravitational search algorithm with DG penetration," IEEE Trans. On Industry Applications, Vol.54, no. 2, March/APRIL, 2018.
3. J.P. Sharma, Vibhor Chauhan and HR Kamath, "Modelling and Analysis of solid State Fault Current Limiter," International Journal of Electrical, Electronics and Data Communication, vol.2, No.6, pp.9-13, June 2014.
4. V.K. Stood and S. Shahabur Alam, "3-phase Fault Current Limiter for distribution systems". IEEE International conference on Power Electronics, Drives 2006.
5. M.M.A. Salama, H. Temraz, A.Y. Chikhani and M.A. Bayoumi, "Fault-Current Limiter with thyristor - controlled impedance", IEEE Trans. on Power Delivery, Vol. 8, No. 3, July.
6. Fabio Tosato and Stefano Quaia, "Reducing Voltage Sags through fault current limitation", IEEE Trans. on Power Delivery, Vol.16, No.1, January 2001.
7. A. Urdaneta, R. Nadira, and L.G. Perez Jimenez, "Optimal coordination of directional overcurrent relays in interconnected power systems," IEEE Trans. on Power Delivery, vol.3, no.3, pp.903-911, July. 1988.
8. P.P. Bedekar, S.R. Bhide, and V.S. Kale, "Coordination of overcurrent relays in distribution system using linear programming problem," in Proc. Int. Conf. Control Autom. Commun. Energy Conserv., Jun. 4-6, 2009.
9. A. Srivastava, J.M. Tripathi, S.R. Mohanty, and N. Kishor, "A simulation based comparative study of optimization techniques for relay coordination with distributed generation," in Proc. IEEE Student Conf. Eng. Syst., Allahabad, India, May 2014.
10. S. Mirjalili and S.Z.M. Hashim, "A new hybrid PSO-GSA algorithm for function optimization," in Proc. Int. Conf. Comput. Inf. Appl., 2010, pp.374-377.
11. M. J. Damborg et al., "Computer aided transmission protection system design, Part I: algorithms," IEEE Trans. Power App. Syst., vol. PAS-103, no.1, pp.51-59, Jan. 1984.
12. A. Srivastava, J. Mani Tripathi and S.R. Mohanty & Bhagabat Panda (2016), "Over current relay coordination with distributed generation using hybrid PSO-GSA," Electric Power components and systems, 44:5, 506-517.